

4.2 Output equation of Induction motor

Output equation is the mathematical expression which gives the relation between the various physical and electrical parameters of the electrical machine.

In an induction motor the output equation can be obtained as follows Consider an 'm' phase machine, with usual notations

Output Q in kW = Input x efficiency

Input to motor = $mV_{ph} I_{ph} \cos \Phi \times 10^{-3}$ kW

For a 3 Φ machine $m = 3$,

Input to motor = $3V_{ph} I_{ph} \cos \Phi \times 10^{-3}$ kW Assuming

$$\begin{aligned} V_{ph} = E_{ph}, V_{ph} = E_{ph} &= 4.44 f \Phi T_{ph} K_w \\ &= 2.22 f \Phi Z_{ph} K_w \end{aligned}$$

$$f = PNs/120 = Pn_s/2,$$

$$\text{Output} = 3 \times 2.22 \times Pn_s/2 \times \Phi Z_{ph} K_w I_{ph} \eta \cos \Phi \times 10^{-3} \text{ kW}$$

$$\text{Output} = 1.11 \times P\Phi \times 3I_{ph} Z_{ph} \times n_s K_w \eta \cos \Phi \times 10^{-3} \text{ kW},$$

$$P\Phi = B_{av}\pi DL, \text{ and } 3I_{ph} Z_{ph}/\pi D = q$$

$$\text{Output to motor} = 1.11 \times B_{av}\pi DL \times \pi Dq \times n_s K_w \eta \cos \Phi \times 10^{-3} \text{ kW}$$

$$Q = (1.11 \pi^2 B_{av} q K_w \eta \cos \Phi \times 10^{-3}) D^2 L n_s \text{ kW}$$

$$Q = (11 B_{av} q K_w \eta \cos \Phi \times 10^{-3}) D^2 L n_s \text{ kW} \text{ Therefore}$$

$$\text{Output } Q = C_o D^2 L n_s \text{ kW}$$

$$\text{where } C_o = (11 B_{av} q K_w \eta \cos \Phi \times 10^{-3})$$

V_{ph} = phase voltage;

I_{ph} = phase current

Z_{ph} = no of conductors/phase

T_{ph} = no of turns/phase

N_s = Synchronous speed in rpm

n_s = synchronous speed in rps

p = no of poles,

q = Specific electric loading

Φ = air gap flux/pole;

B_{av} = Average flux density

k_w = winding factor.

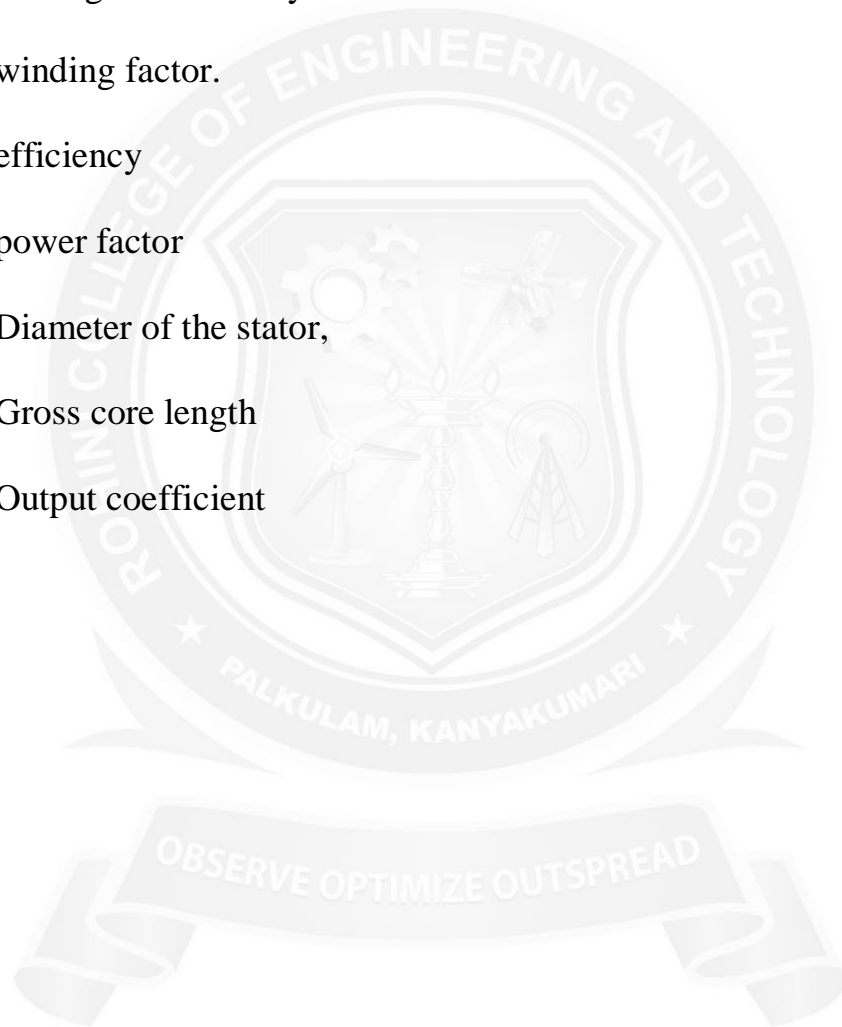
η = efficiency

$\cos\Phi$ = power factor

D = Diameter of the stator,

L = Gross core length

C_o = Output coefficient



4.3 Choice of specific loadings

Specific magnetic loading:

Following are the factors which influences the performance of the machine.

(i) Iron loss:

A high value of flux density in the air gap leads to higher value of flux in the iron parts of the machine which results in increased iron losses and reduced efficiency.

(ii) Voltage:

When the machine is designed for higher voltage space occupied by the insulation becomes more thus making the teeth smaller and hence higher flux density in teeth and core.

(iii) Transient short circuit current:

A high value of gap density results in decrease in leakage reactance and hence increased value of armature current under short circuit conditions.

(iv) Stability:

The maximum power output of a machine under steady state condition is indirectly proportional to synchronous reactance. If higher value of flux density is used it leads to smaller number of turns per phase in armature winding. This results in reduced value of leakage reactance and hence increased value of power and hence increased steady state stability.

(v) Parallel operation:

The satisfactory parallel operation of synchronous generators depends on the synchronizing power. Higher the synchronizing power higher will be the ability of the machine to operate in synchronism. The synchronizing power is inversely proportional to the synchronous reactance and hence the machines designed with higher value air gap flux density will have better ability to operate in parallel with other machines.

Specific Electric Loading:

Following are the some of the factors which influence the choice of specific electric loadings.

(i) Copper loss:

Higher the value of q larger will be the number of armature of conductors which results in higher copper loss. This will result in higher temperature rise and reduction in efficiency.

(ii) Voltage:

A higher value of q can be used for low voltage machines since the space required for the insulation will be smaller.

(iii) Synchronous reactance:

High value of q leads to higher value of leakage reactance and armature reaction and hence higher value of synchronous reactance. Such machines will have poor voltage regulation, lower value of current under short circuit condition and low value of steady state stability limit and small value of synchronizing power.

(iv) Stray load losses:

With increase of q stray load losses will increase. Values of specific magnetic and specific electric loading can be selected from Design Data Hand Book for salient and non-salient pole machines.

Separation of D and L:

Inner diameter and gross length of the stator can be calculated from D^2L product obtained from the output equation. To separate suitable relations are assumed between D and L depending upon the type of the generator. Salient pole machines: In case of salient pole machines either round or rectangular pole construction is employed. In these types of machines, the diameter of the machine will be quite larger than the axial length.