

MONOSTABLE MULTIVIBRATOR

- Figure 1 shows the circuit diagram of a collector-to-base coupled (simply called collector-coupled) monostable multivibrator using n-p-n transistors. The collector of Q_2 is coupled to the base of Q_1 by a resistor R_1 (dc coupling) and the collector of Q_1 is coupled to the base of Q_2 by a capacitor C_1 (ac coupling). C_1 is the commutating capacitor introduced to increase the speed of operation. The base of Q_1 is connected to $-V_{BB}$ through a resistor R_2 , to ensure that Q_1 is cut off under quiescent conditions.
- The base of Q_2 is connected to V_{CC} through R_3 to ensure that Q_2 is ON under quiescent conditions. In fact, R_3 may be returned to even a small positive voltage but connecting it to V_{CC} is advantageous.
- The circuit parameters are selected such that under quiescent conditions, the monostable multivibrator finds itself in its permanent stable state with Q_2 ON (i.e. in saturation) and Q_1 OFF (i.e. in cut-off)- The multivibrator may be induced to make a transition out of its stable state by the application of a negative trigger at the base of Q_2 or at the collector of Q_1 . Since the triggering signal is applied to only one device and not to both the devices simultaneously, unsymmetrical triggering is employed.
- When a negative signal is applied at the base of Q_2 at $t = 0$, due to regenerative action Q_2 goes to OFF state and Q_1 goes to ON state. When Q_1 is ON, a current I_1 flows through its R_C and hence its collector voltage drops suddenly by $I_1 R_C$. This drop will be instantaneously

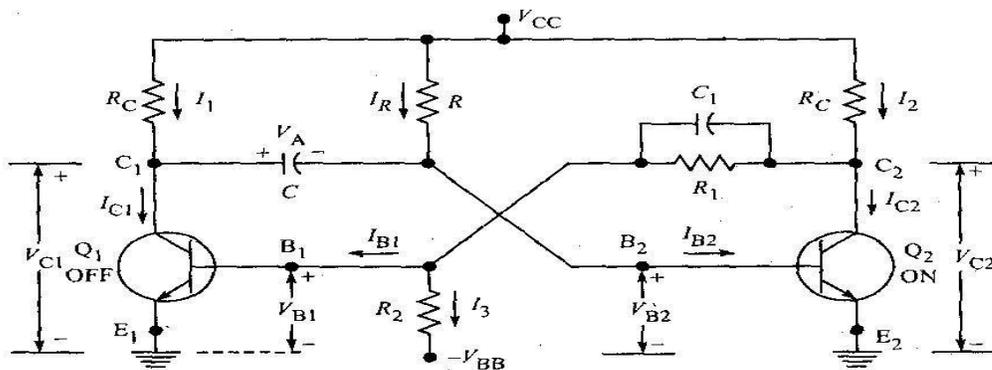


Figure 1 Circuit diagram of a collector-coupled monostable multivibrator.

transmitted through the coupling capacitor C to the base of Q_2 . So at $t = 0^+$, the base voltage of Q_2 is

$$V_{BE}(\text{sat}) - I_1 R_C$$

- The circuit cannot remain in this state for a long time (it stays in this state only for a finite time T) because when Q_1 conducts, the coupling capacitor C charges from V_{CC} through the conducting transistor Q_1 and $(R + R_o)C \approx RC$,

hence the potential at the base of Q_2 rises exponentially with a time constant

- where R_0 is the conducting transistor output impedance including the resistance R_C . When it passes the cut-in voltage V_y of Q_2 (at a time $t = T$), a regenerative action takes place turning Q_1 OFF and eventually returning the multivibrator to its initial stable state.
- The transition from the stable state to the quasi-stable state takes place at $t = 0$, and the reverse transition from the quasi-stable state to the stable state takes place at $t = T$. The time T for which the circuit is in its quasi-stable state is also referred to as the delay time, and also as the gate width, pulse width, or pulse duration. The delay time may be varied by varying the time constant $t(= RC)$.

Expression for the gate width T of a monostable multivibrator neglecting the

reverse saturation current /CBO

- Figure 4.42(a) shows the waveform at the base of transistor Q2 of the monostable multivibrator shown in Figure 4.41.
- For $t < 0$, Q2 is ON and so $v_{B2} = V_{BE(sat)}$. At $t = 0$, a negative signal applied brings Q2 to OFF state and Q1 into saturation. A current I_1 flows through R_C of Q1 and hence v_{C1} drops abruptly by $I_1 R_C$ volts and so v_{B2} also drops by $I_1 R_C$ instantaneously. So at $t = 0$, $v_{B2} = V_{BE(sat)} - I_1 R_C$. For $t > 0$, the capacitor charges with a time constant RC , and hence the base voltage of Q2 rises exponentially towards V_{CC} with the same time constant. At $t = T$, when this base voltage rises to the cut-in voltage level V_γ of the transistor, Q2 goes to ON state, and Q1 to OFF state and the pulse ends.

In the interval $0 < t < T$, the base voltage of Q2, i.e. v_{B2} is given by

$$v_{B2} = V_{CC} - (V_{CC} - \{V_{BE(sat)} - I_1 R_C\})e^{-t/\tau}$$

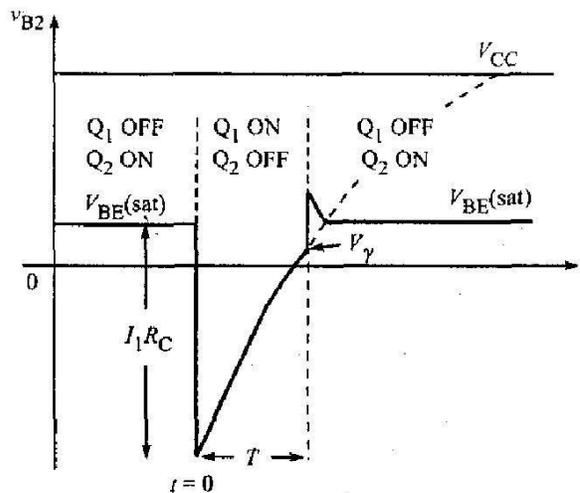


Figure 4.42(a) Voltage variation at the base of Q2 during the quasi-stable state (neglecting I_{CBO})

But $I_1 R_C = V_{CC} - V_{CE}(\text{sat})$ (because at $t = 0^-$, $v_{C1} = V_{CC}$ and at $t = 0^+$, $v_{C1} = V_{CE}(\text{sat})$)

$$\begin{aligned} \therefore v_{B2} &= V_{CC} - [V_{CC} - \{V_{BE}(\text{sat}) - (V_{CC} - V_{CE}(\text{sat}))\}]e^{-t/\tau} \\ &= V_{CC} - [2V_{CC} - \{V_{BE}(\text{sat}) + V_{CE}(\text{sat})\}]e^{-t/\tau} \end{aligned}$$

At $t = T$, $v_{B2} = V_\gamma$

$$\therefore V_\gamma = V_{CC} - [2V_{CC} - \{V_{CE}(\text{sat}) + V_{BE}(\text{sat})\}]e^{-T/\tau}$$

$$\text{i.e. } e^{T/\tau} = \frac{2V_{CC} - [V_{CE}(\text{sat}) + V_{BE}(\text{sat})]}{V_{CC} - V_\gamma}$$

$$\therefore \frac{T}{\tau} = \frac{\ln \left[2 \left(V_{CC} - \frac{V_{CE}(\text{sat}) + V_{BE}(\text{sat})}{2} \right) \right]}{V_{CC} - V_\gamma}$$

$$\text{i.e. } T = \tau \ln 2 + \tau \ln \frac{V_{CC} - \frac{V_{CE}(\text{sat}) + V_{BE}(\text{sat})}{2}}{V_{CC} - V_\gamma}$$

Normally for a transistor, at room temperature, the cut-in voltage is the average of the saturation junction

voltages for either Ge or Si transistors, i.e. $V_\gamma = \frac{V_{CE}(\text{sat}) + V_{BE}(\text{sat})}{2}$

Neglecting the second term in the expression for T

$$T = \tau \ln 2$$

$$\text{i.e. } T = (R + R_o)C \ln 2 = 0.693(R + R_o)C$$

but for a transistor in saturation $R_a \ll R$.

Gate width, $T = 0.693RC$

- The larger the V_{CC} is, compared to the saturation junction voltages, the more accurate the result is.

The gate width can be made very stable (almost independent of transistor characteristic supply voltages, and resistance values) if Q1 is driven into saturation during the quasi-stable state.

Expression for the gate width of a monostable multivibrator considering the

reverse saturation current /CBO

- In the derivation of the expression for gate width T above, we neglected the

effect of reverse saturation current I_{CBO} on the gate width T . In fact, as the temperature increases, reverse saturation current increases and the gate width decreases.

- In the quasi-stable state when Q_2 is OFF, I_{CBO} flows out of its base through R to the supply V_{CC} . Hence the base of Q_2 will be not at V_{CC} but at $V_{CC} + I_{CBO}R$. If the junction of the base of Q_2 with the resistor R is disconnected from the junction of the base of Q_2 with the resistor R . It therefore appears that the capacitor C in effect charges through R from a source $V_{CC} + I_{CBO}R$. See Figure 4.42(b).

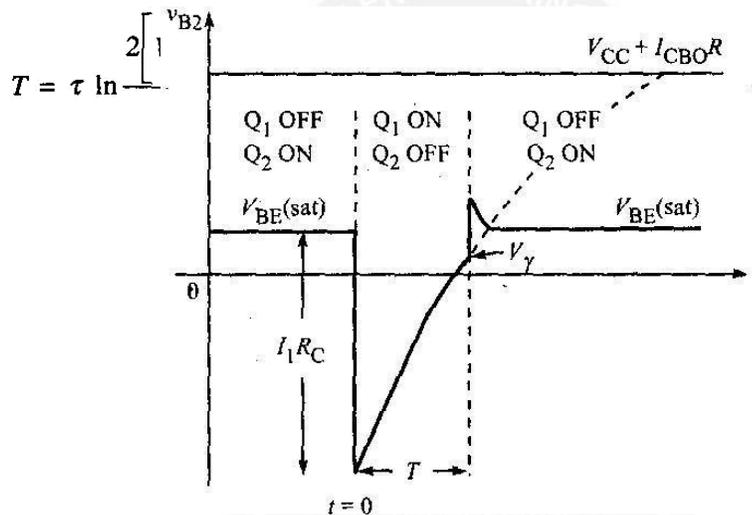


Figure 4.42(b) Voltage variation at the base of Q_2 during the quasistable state. So, the expression for the voltage at the base of Q_2 is given by

$$v_{B2} = (V_{CC} + I_{CBO}R) - [(V_{CC} + I_{CBO}R) - (V_{BE}(sat) - I_1R_C)]e^{-t/\tau}$$

$$= (V_{CC} + I_{CBO}R) - [(V_{CC} + I_{CBO}R) - (V_{BE}(sat) - (V_{CC} - V_{CE}(sat)))]e^{-t/\tau}$$

At $t = T$, $v_{B2} = V_\gamma$

$$\therefore V_\gamma = V_{CC} + I_{CBO}R - [2V_{CC} + I_{CBO}R - (V_{CE}(sat) + V_{BE}(sat))]e^{-T/\tau}$$

$$\therefore e^{T/\tau} = \frac{2V_{CC} + I_{CBO}R - (V_{CE}(sat) + V_{BE}(sat))}{V_{CC} + I_{CBO}R - V_\gamma}$$

(considering

Neglecting the junction voltages and the cut-in voltage of the transistor,

$$T = \tau \ln \frac{2 \left[V_{CC} + \frac{I_{CBO} R}{2} \right]}{V_{CC} + I_{CBO} R}$$

$$= \tau \ln 2 + \tau \ln \frac{1 + \frac{\phi}{2}}{1 + \phi}, \quad \text{where } \phi = \frac{I_{CBO} R}{V_{CC}}$$

$$T = \tau \ln 2 - \tau \ln \frac{1 + \phi}{1 + \frac{\phi}{2}}$$

- Since I_{CBO} increases with temperature, we can conclude that the delay time T decreases as temperature increases.

Waveforms of the collector-coupled monostable multivibrator

- The waveforms at the collectors and bases of both the transistors Q_1 and Q_2 of the monostable multivibrator of Figure 4.41 are shown in Figure 4.44. The triggering signal is applied at $t = 0$, and the reverse transition occurs at $t = T$.

The stable state. For $t < 0$, the monostable circuit is in its stable state with Q_2 ON and Q_1 OFF. Since Q_2 is ON, the base voltage of Q_2 is $v_{B2} = V_{BE2}(\text{sat})$ and the collector voltage of Q_2 is $v_{C2} = V_{CE2}(\text{sat})$. Since Q_1 is OFF, there is no current in R_C of Q_1 and its base voltage must be negative. Hence the voltage at the collector of Q_1 is, $v_{C1} = V_{CC}$

and the voltage at the base of Q_1 using the superposition theorem is

$$v_{B1} = -V_{BB} \frac{R_1}{R_1 + R_2} + V_{CE2}(\text{sat}) \frac{R_2}{R_1 + R_2}$$

The quasi-stable state.

- A negative triggering signal applied at $t = 0$ brings Q_2 to OFF state and Q_1 to ON state.

A current I_C flows in R_C of Q_1 . So, the collector voltage of Q_1 drops suddenly by $I_C R_C$ volts. Since the

voltage across the coupling capacitor C cannot change instantaneously, the

voltage at the base of Q2 also drops by $I_1 R_C$, where $I_1 R_C = V_{CC} - V_{CE2}(\text{sat})$. Since Q1 is ON,

$$v_{B1} = V_{BE1}(\text{sat}) \quad \text{and} \quad v_{C1} = V_{CE1}(\text{sat})$$

$$\text{Also, } v_{B2} = V_{BE2}(\text{sat}) - I_1 R_C \quad \text{and} \quad v_{C2} = V_{CC} \frac{R_1}{R_1 + R_C} + V_{BE1}(\text{sat}) \frac{R_C}{R_1 + R_C}$$

In the interval $0 < t < T$, the voltages V_{C1} , V_{B1} and V_{C2} remain constant at their values at $t = 0$, but the voltage at the base of Q2, i.e. v_{B2} rises exponentially towards V_{CC} with a time constant, $t - RC$, until at $t = T$, v_{B2} reaches the cut-in voltage V_X of the transistor.

Waveforms for $t > T$. At $t = T$, reverse transition takes place. Q2 conducts and Q1 is cut-off. The collector voltage of Q2 and the base voltage of Q1 return to their voltage levels for $t < 0$. The voltage v_{C1}

now rises abruptly since Q1 is OFF. This increase in voltage is transmitted to the base of Q2 and drives Q2 heavily into saturation. Hence an overshoot develops in v_{B2} at $t = T^+$, which decays as the capacitor recharges because of the base current. The magnitude of the base current may be calculated as follows.

Replace the input circuit of Q2 by the base spreading resistance r_{BB} in series with the voltage $V_{BE}(\text{sat})$ as shown in Figure 4.43. Let I_B be the base current at $t = T^+$.

The current in R may be neglected compared to I_B .

From Figure 4.43,

$$V_{BE} = I_B r'_{BB} + V_{BE}(\text{sat}) \quad \text{and} \quad V_C = V_{CC} - I_B R_C - V_{BE}$$

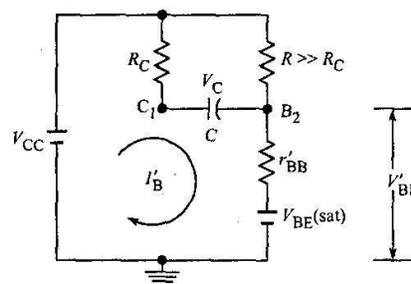


Figure 4.43 Equivalent circuit for calculating the overshoot at base of Q3.

The jumps in voltages at B2 and C1 are, respectively, given by

$$\delta = V'_{BE} - V_{\gamma} = I'_B r'_{BB} + V_{BE(sat)} - V_{\gamma} \quad \text{and} \quad \delta' = V_{CC} - V_{CE(sat)} - I'_B R_C$$

Since C1 and B2 are connected by a capacitor C and since the voltage across the capacitor cannot change instantaneously, these two discontinuous voltage changes δ and δ' must be equal.

Equating them,

$$I'_B r'_{BB} + V_{BE(sat)} - V_{\gamma} = V_{CC} - V_{CE(sat)} - I'_B R_C$$

$$I'_B = \frac{V_{CC} - V_{BE(sat)} - V_{CE(sat)} + V_{\gamma}}{R_C + r'_{BB}}$$

v_{B2} and v_{C1} decay to their steady-state values with a time constant $\tau' = (R_C + r'_{BB})C$

